

16-Bit, 170/200-MSPS Analog-to-Digital Converters

Check for Samples: [ADS5484](https://commerce.ti.com/stores/servlet/SCSAMPLogon?storeId=10001&langId=-1&catalogId=10001&reLogonURL=SCSAMPLogon&URL=SCSAMPSBDResultDisplay&GPN1=ads5484) [ADS5485](https://commerce.ti.com/stores/servlet/SCSAMPLogon?storeId=10001&langId=-1&catalogId=10001&reLogonURL=SCSAMPLogon&URL=SCSAMPSBDResultDisplay&GPN1=ads5485)

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- **• Data Acquisition • On-Chip High Impedance Analog Buffer**
- *<u>Efficient DDR LVDS-Compatible Outputs</u>*
- **• Power-Down Mode: 70 mW**
- **• Pin-for-Pin with ADS5483/5482/5481, 135/105/80-MSPS ADCs**
- **• QFN-64 PowerPAD™ Package (9 mm × 9 mm footprint)**
- **• Industrial Temperature Range: –40°C to 85°C**

¹FEATURES APPLICATIONS

- **²³• 170/200-MSPS Sample Rates • Wireless Infrastructure**
- **• 16-Bit Resolution, 78 dBFS Noise Floor • Test and Measurement Instrumentation**
- **• SFDR = 95 dBc • Software-Defined Radio**
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	-
	- **• Radar**
	- **• Medical Imaging**

DESCRIPTION

The ADS5484/ADS5485 (ADS548x) is a 16-bit family of analog-to-digital converters (ADCs) that operate from both a 5-V supply and 3.3-V supply while providing LVDS-compatible digital outputs. The ADS548x integrated analog input buffer isolates the internal switching of the onboard track and hold (T & H) from disturbing the signal source while providing a high-impedance input. An internal reference generator is provided to simplify the system design. Internal dither is available to improve SFDR. These devices are drop-in compatible to the ADS5483/5482/5481, creating a pin-compatible family from 80 – 200 MSPS. Designed for highest total ENOB, the ADS548x family has outstanding low noise performance and spurious-free dynamic range.

The ADS548x family is available in a QFN-64 PowerPAD package. The devices are built on Texas Instruments complementary bipolar process (BiCom3) and are specified over the full industrial temperature range (–40°C to 85°C).

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 $\sqrt{2}$

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

B0095-03

(1) For the most current product and ordering information see the Package Option Addendum located at the end of this document, or see the TI website at www.ti.com..

ABSOLUTE MAXIMUM RATINGS(1)

Over operating free-air temperature range, unless otherwise noted.

(1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied. Kirkendall voidings and current density information for calculation of expected lifetime are available upon request.

THERMAL CHARACTERISTICS(1)

(1) Using 49 thermal vias (7 × 7 array). See PowerPAD Package in the Application Information section.

RECOMMENDED OPERATING CONDITIONS

ELECTRICAL CHARACTERISTICS (ADS5484, ADS5485)

Typical values at $T_A = 25^{\circ}$ C: minimum and maximum values over full temperature range $T_{MIN} = -40^{\circ}$ C to $T_{MAX} = 85^{\circ}$ C, sampling rate = max rated, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, -1 dBFS differential input, and $3-V_{PP}$ differential clock, unless otherwise noted.

ELECTRICAL CHARACTERISTICS (ADS5484, ADS5485) (continued)

Typical values at T_A = 25°C: minimum and maximum values over full temperature range T_{MIN} = –40°C to T_{MAX} = 85°C, sampling rate = max rated, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, –1 dBFS differential input, and $3-V_{PP}$ differential clock, unless otherwise noted.

ELECTRICAL CHARACTERISTICS (ADS5484, ADS5485) (continued)

Typical values at T_A = 25°C: minimum and maximum values over full temperature range T_{MIN} = –40°C to T_{MAX} = 85°C, sampling rate = max rated, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, –1 dBFS differential input, and $3-V_{PP}$ differential clock, unless otherwise noted.

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TIMING INFORMATION

Dx_y_P/M are LVDS outputs that have two bits per pair (EVEN and ODD). The values for x and y are 0_1, 2_3, 4_5, ... 14_15.

T0158-02

Figure 1. Timing Diagram

TIMING CHARACTERISTICS(1)

Typical values at T_A = 25°C: minimum and maximum values over full temperature range T_{MIN} = -40°C to T_{MAX} = 85°C, sampling rate = max rated, 50% clock duty cycle, AVDD5 = 5 V, AVDD3 = 3.3 V, DVDD3 = 3.3 V, and 3-V_{PP} differential clock, unless otherwise noted.

(1) Timing parameters are assured by design or characterization, but not production tested.
(2) DRY and DATA are updated on the rising edge of CLK input. The latency must be adde

DRY and DATA are updated on the rising edge of CLK input. The latency must be added to t_{DATA} to determine the overall propagation delay.

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Table 2. PIN FUNCTIONS

TYPICAL CHARACTERISTICS

At $T_A = 25^{\circ}$ C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

ADS5484 - 170-MSPS Typical Data

Plots in this section are with a clock of 170 MSPS, unless otherwise specified. **ADS5484 SPECTRAL PERFORMANCE ADS5484 SPECTRAL PERFORMANCE**

Figure 4. Figure 5.

Figure 2. Figure 3. ADS5484 SPECTRAL PERFORMANCE ADS5484 SPECTRAL PERFORMANCE vs vs

TYPICAL CHARACTERISTICS (continued)

At T_A = 25°C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

TYPICAL CHARACTERISTICS (continued)

At T_A = 25°C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

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TYPICAL CHARACTERISTICS (continued)

vs vs

vs vs

At T_A = 25°C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

ADS5485 - 200-MSPS Typical Data

Plots in this section are with a clock of 200 MSPS, unless otherwise specified. **ADS5485 SPECTRAL PERFORMANCE ADS5485 SPECTRAL PERFORMANCE**

f − Frequency − MHz −120 −110 −100 −90 −80 −70 −60 −50 −40 −30 −20 −10 0 0 10 20 30 40 50 60 70 80 90 100 Amplitude − dB $G018$ $SFDR = 93$ dBc $SINAD = 75.7$ dBFS SNR = 75.8 dBFS $THD = 97$ dBc **FFT for 10-MHz INPUT SIGNAL FFT for 70-MHz INPUT SIGNAL**

Figure 13. Figure 14.

ADS5485 SPECTRAL PERFORMANCE ADS5485 SPECTRAL PERFORMANCE

Figure 15. Figure 16.

−20 −10 Ω $SFDR = 88$ dBc $SINAD = 74.7$ dBFS $SNR = 75$ dBFS

TYPICAL CHARACTERISTICS (continued)

At T_A = 25°C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

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TYPICAL CHARACTERISTICS (continued)

At T_A = 25°C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

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TYPICAL CHARACTERISTICS (continued)

At T_A = 25°C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

Typical Data, Valid for Both ADS5484/5485

Plots in this section are valid for either device or otherwise have combined plots. **NORMALIZED GAIN RESPONSE**

Figure 24. Figure 25.

INOISE HISTOGRAM WITH INPUTS SHORTED

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TYPICAL CHARACTERISTICS (continued)

At $T_A = 25^{\circ}$ C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

SNR

Figure 28.

TYPICAL CHARACTERISTICS (continued)

At $T_A = 25^{\circ}$ C, sampling rate = max rated, 50% clock duty cycle, 3-V_{PP} differential sinusoidal clock, analog input amplitude = -1 dBFS, AVDD5 = 5 V, AVDD3 = 3.3 V, and DVDD3 = 3.3 V, unless otherwise noted.

SFDR

Figure 29.

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APPLICATIONS INFORMATION

Theory of Operation

The ADS5484/ADS5485 (ADS548x) is a 16-bit, 170/200-MSPS family of monolithic pipeline ADCs. The bipolar analog core operates from 5-V and 3.3-V supplies, while the output uses a 3.3-V supply to provide LVDS-compatible outputs. Prior to the track-and-hold, the analog input signal passes through a high-performance bipolar buffer. The buffer presents a high and consistent impedance to the analog inputs. The buffer isolates the board circuitry external to the ADC from the sampling glitches caused by the track-and-hold in the ADC. The conversion process is initiated by the falling edge of the external input clock. At that instant, the differential input signal is captured by the input track-and-hold, and the input sample is converted sequentially by a series of lower resolution stages, with the outputs combined in a digital correction logic block. Both the rising and the falling clock edges are used to propagate the sample through the pipeline every half clock cycle. This process results in a data latency of 4.5 clock cycles, after which the output data are available as a 16-bit parallel word, coded in offset binary format.

Input Configuration

The analog input for the ADS548x consists of an analog pseudo-differential buffer followed by a bipolar transistor T & H. The analog buffer isolates the source driving the input of the ADC from any internal switching and presents a high impedance to drive at high input frequencies, as compared to an ADC without a buffered input. The input common-mode is set internally through a 1000-Ω resistor connected from 3.1 V to each of the inputs. This configuration results in a differential input impedance of 2 kΩ at 0 Hz. [Figure](#page-18-0) 30 estimates the package parasitics before soldering to a board. Each board is different, but soldering to the board will likely add 1 – 2 pF to the input capacitance.

Figure 30. Analog Input Circuit (unsoldered package)

For a full-scale differential input, each of the differential lines of the input signal (pins 11 and 12) swings symmetrically between (3.1 V + 0.75 V) and (3.1 V – 0.75 V). This range means that each input has a maximum signal swing of 1.5 V_{PP} for a total differential input signal swing of 3 V_{PP}. Operation below 3 V_{PP} is allowable, with the characteristics of performance versus input amplitude demonstrated in [Figure](#page-10-0) 8 through [Figure](#page-11-0) 10. For instance, for performance at 2 V_{PP} rather than 3 V_{PP} , refer to the SNR and SFDR at –3.5 dBFS (0 dBFS =

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 $3 V_{\rm PP}$). The maximum swing is determined by the internal reference voltage generator, eliminating the need for any external circuitry for this purpose. The primary degradation visible if the maximum amplitude is kept to 2 V_{PP} is \sim 3 dBc of SNR compared to using 3 V_{PP} , while SFDR is the same or even improved. The smaller input signal also possibly helps any components in the signal chain prior to the ADC to be more linear and provide better distortion.

The ADS548x performs optimally when the analog inputs are driven differentially. The circuit in [Figure](#page-19-0) 31 shows one possible configuration using an RF transformer with termination either on the primary or on the secondary of the transformer. If voltage gain is required, a step-up transformer can be used.

Figure 31. Converting a Single-Ended Input to a Differential Signal Using an RF Transformer

Dither

The ADS548x family of devices contain a dither option that is enabled via the DITHEREN pin. Dither is a technique applied to convert small static errors in the converter to dynamic errors, which look similar to white noise in the output. It improves the harmonics that are a function of the static errors. The dither is a low level and is only indicated in the output waveform as wideband noise that may slightly degrade the SNR. It is recommended that users should allow the capability to enable/disable it in the event they would like to compare the results during their evaluation. In addition to the plots on the first page of the data sheet, [Figure](#page-10-0) 8 through [Figure](#page-11-0) 10 and [Figure](#page-13-0) 19 through [Figure](#page-14-0) 21 show the minor differences of dither on/off when studied.

External Voltage Reference

For systems that require the analog signal gain to be adjusted or calibrated, this can be performed by using an external reference. The dependency on the signal amplitude to the value of the external reference voltage is characterized typically by [Figure](#page-19-1) 32 (VREF = 1.2 V is normalized to 0 dB as this is the internal reference voltage). As can be seen in the linear fit, this equates to approximately ~1 dB of signal adjustment per 100 mV of reference adjustment. The range of allowable variation depends on the analog input amplitude that is applied to the inputs and the desired spectral performance, as can be seen in the performance versus external reference graphs in [Figure](#page-19-1) 33 and [Figure](#page-20-0) 34.

For dc-coupled applications that use the VCM pin of the ADS548x as the common mode of the signal in the analog signal gain path prior to the ADC inputs, [Figure](#page-20-1) 36 indicates little change in VCM output as VREF is externally adjusted. The VCM output is buffered with a 2 - $kΩ$ series output resistor.

The method for disabling the internal reference for use with an external reference is described in [Table](#page-26-1) 5 . The following VREF adjustment graphs were collected using the ADS5483, but are indicative of the behavior of the ADS5484/5485. The absolute performance may differ from device to device, but the relative characteristics are valid.

Figure 32. Signal Gain Adjustment versus External Figure 33. SFDR versus External VREF and AIN Reference (VREF)

Figure 34. SNR versus External VREF and AIN Figure 35. Total Power Consumption versus

 $\overline{\text{A}}$ dBFS

 $dBFS$

 $M_N = -6$ dBFS

 $A_{IN} = -2$ dBFS

 $A_{IN} = -7$ dBFS

75

80

85

SFDR − dBc

90

95

100

External VREF

Figure 36. VCM Pin Output versus External VREF

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 $f_S = 135$ MSPS $f_{IN} = 30$ MHz Dither Enabled Signal Amplitude Relative to Adjusted Fullscale

 $A_{IN} = -10$ dBFS

 $A_{IN} = -4$ dBFS

Clock Inputs

The ADS548x equivalent clock input circuit is shown in [Figure](#page-21-0) 37. The clock inputs can be driven with either a differential clock signal or a single-ended clock input, but differential is highly recommended. The characterization of the ADS548x is typically performed with a 3-V_{PP} differential clock, but the ADC performs well with a differential clock amplitude down to -1 V_{PP}, as shown in [Figure](#page-22-0) 39 and Figure 40. The performance is optimized when the clock amplitude is kept above 2 V_{PP} . The clock amplitude becomes more of a factor in performance as the analog input frequency increases. When single-ended clocking is a necessity, it is best to connect CLKM to ground with a 0.01-μF capacitor, while CLKP is ac-coupled with a 0.01-μF capacitor to the clock source, as shown in [Figure](#page-21-1) 38.

Figure 37. Clock Input Circuit

Figure 38. Single-Ended Clock

For jitter-sensitive applications, the use of a differential clock has some advantages at the system level. The differential clock allows for common-mode noise rejection at the printed circuit board (PCB) level. With a differential clock, the signal-to-noise ratio of the ADC is better for jitter-sensitive, high-frequency applications because the board level clock jitter is superior.

The sampling process is more sensitive to jitter using high analog input frequencies or slow clock frequencies. Large clock amplitude levels are recommended when possible to reduce the indecision (jitter) in the ADC clock input buffer. Whenever possible, the ideal combination is a differential clock with large signal swing $(-1 - 3 \text{ V}_{\text{PP}})$. [Figure](#page-22-1) 41 demonstrates a recommended method for converting a single-ended clock source into a differential clock; it is similar to the configuration found on the evaluation board and was used for much of the characterization. See also Clocking High Speed Data Converters ([SLYT075](http://www.ti.com/lit/SLYT075)) for more details.

Figure 41. Differential Clock

The common-mode voltage of the clock inputs is set internally to ~2 V using internal 0.5-k Ω resistors. It is recommended to use ac coupling, but if this scheme is not possible, the ADS548x features good tolerance to clock common-mode variation (as shown in [Figure](#page-22-2) 42 and [Figure](#page-22-2) 43). The internal ADC core uses both edges of the clock for the conversion process. Ideally, a 50% duty-cycle clock signal should be provided. Performance degradation as a result of duty cycle can be seen in [Figure](#page-23-0) 44.

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Figure 42. SFDR versus Clock Common-Mode Figure 43. SNR versus Clock Common-Mode

Voltage Voltage

Figure 44. SFDR vs Clock Duty Cycle

The ADS5484 is capable of achieving 75.7 dBFS SNR at 130 MHz of analog input frequency. In order to achieve the SNR at 130 MHz the clock source rms jitter (at the ADC clock input pins) must be at most 184 fsec in order for the total rms jitter to be 201 fsec due to internal ADC aperture jitter of ~80 fsec. A summary of maximum recommended rms clock jitter as a function of analog input frequency for the ADS5484 is provided in [Table](#page-23-1) 3. The equations used to create the table are presented and can be used to estimate required clock jitter for virtually any pipeline ADC, but in particular, the ADS5481/5482/5483/5484/5485 family.

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(2)

[Equation](#page-24-0) 1 and [Equation](#page-24-1) 2 are used to estimate the required clock source jitter.

$$
SNR (dBc) = -20 \times LOG10 (2 \times \pi \times f_{IN} \times j_{TOTAL})
$$
\n(1)

 $j_{\text{TOTAL}} = (j_{\text{ADC}}^2 + j_{\text{CLOCK}}^2)^{1/2}$

where:

 j_{TOTAI} = the rms summation of the clock and ADC aperture jitter;

 j_{ADC} = the ADC internal aperture jitter which is located in the data sheet;

 j_{CLOCK} = the rms jitter of the clock at the clock input pins to the ADC; and

 f_{IN} = the analog input frequency.

Notice that the SNR is a strong function of the analog input frequency, not the clock frequency. The slope of the clock source edges can have a mild impact on SNR as well and is not taken into account for these estimates. For this reason, maximizing clock source amplitudes at the ADC clock inputs is recommended, though not required (faster slope is desirable for jitter-related SNR). For more information on clocking high-speed ADCs, see Application Note [SLWA034,](http://www.ti.com/lit/SLWA034) Implementing a CDC7005 Low Jitter Clock Solution For High-Speed, High-IF ADC Devices, on the Texas Instruments web site. Recommended clock distribution chips (CDCs) are the TI CDCE72010 and [CDCM7005](http://focus.ti.com/docs/prod/folders/print/cdcm7005.html). Depending on the jitter requirements, a band pass filter (BPF) is sometimes required between the CDC and the ADC. If the insertion loss of the BPF causes the clock amplitude to be too low for the ADC, or the clock source amplitude is too low to begin with, an inexpensive amplifier can be placed between the CDC and the BPF, as its harmonics and wide-band noise are reduced by the BPF.

[Figure](#page-24-2) 45 represents a scenario where an LVCMOS single-ended clock output is used from a TI CDCE72010 with the clock signal path optimized for maximum amplitude and minimum jitter. The jitter of this setup is difficult to estimate and requires a careful phase noise analysis of the clock path. The BPF (and possibly a low-cost amplifier because of insertion loss in the BPF) can improve the jitter between the CDC and ADC when the jitter provided by the CDC is still not adequate. The total jitter at the CDCE72010 output depends largely on the phase noise of the VCXO/VCO selected, as well as from the CDCE72010 itself.

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Consult the [CDCE72010](http://www.ti.com/lit/SCAS858) data sheet for proper schematic and specifications regarding allowable input and output frequency and amplitude ranges.

Figure 45. Optimum Jitter Clock Circuit

Digital Outputs

The ADC provides eight LVDS-compatible, offset binary, DDR data outputs (2 bits per LVDS output driver) and a data-ready LVDS signal (DRY). It is recommended to use the DRY signal to capture the output data of the ADS548x (use as a clock output). DRY is source-synchronous to the DATA outputs and operates at the same frequency, creating a full-rate DDR interface that updates data on both the rising and falling edges of DRY. It is recommended that the capacitive loading on the digital outputs be minimized. Higher capacitance shortens the data-valid timing window. The values given for timing (see [Figure](#page-6-0) 1) were obtained with a 5-pF parasitic board capacitance to ground on each LVDS line. When setting the time relationship between DRY and DATA at the receiving device, it is generally recommended that setup time be maximized, but this partially depends on the setup and hold times of the device receiving the digital data. Since DRY and DATA are coincident, it will likely be necessary to delay either DRY such that DATA setup time is maximized.

The LVDS outputs all require an external 100-Ω load between each output pair in order to meet the expected LVDS voltage levels. For long trace lengths, it may be necessary to place a 100-Ω load on each digital output as close to the ADS548x as possible and another 100-Ω differential load at the end of the LVDS transmission line to terminate the transmission line and avoid signal reflections. The effective load in this case reduces the LVDS voltage levels by half. The current of all LVDS drivers is set externally with a resistor connected between the LVDSB (LVDS bias) pin and ground. Normal LVDS current is 3.5 mA per LVDS pair, set with a 10-kΩ external resistor. For systems with excessive load capacitance on the LVDS lines, reducing the resistor value in order to increase the LVDS bias current is allowed to create a stronger LVDS drive capability. For systems with short traces and minimal loading, increasing the resistor in order to decrease the LVDS current is allowable in order to save power. [Table](#page-25-0) 4 provides a sampling of LVDSB resistor values should deviation from the recommended LVDS output current of 3.5 mA be considered. It is not recommended to exceed the range listed in the table. If the LVDS bias current is adjusted, the differential load resistance should also be adjusted to maintain voltage levels within the specification for the LVDS outputs. The signal integrity of the LVDS lines on the board layout should be scrutinized to ensure proper LVDS signal integrity exists.

Table 4. Setting the LVDS Current Drive

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Power Supplies and Sleep Modes

The ADS548x uses three power supplies. For the analog portion of the design, a 5-V and 3.3-V supply (AVDD5 and AVDD3) are used, while the digital portion uses a 3.3-V supply (DVDD3). The use of low-noise power supplies with adequate decoupling is recommended. Linear supplies are preferred to switched supplies; switched supplies generate more noise that can be coupled to the ADS548x. However, the PSRR value and plot shown in [Figure](#page-26-0) 46 were obtained without bulk supply decoupling capacitors. When bulk (0.1-μF) decoupling capacitors are used near the supply pins, the board-level PSRR is much higher than the stated value for the ADC. The user may be able to supply power to the device with a less-than-ideal supply and still achieve good performance. It is not possible to make a single recommendation for every type of supply and level of decoupling for all systems. If the noise characteristics of the available supplies are understood, a study of the PSRR data for the ADS548x may provide the user with enough information to select noisy supplies if the performance is still acceptable within the frequency range of interest. The power consumption of the ADS548x does not change substantially over clock rate or input frequency.

Figure 46. PSRR versus Supply Injected Frequency

Two separate sleep modes are offered. They are differentiated by the amount of power consumed and the time it takes for the ADC to wake-up from sleep. The light sleep mode consumes 605 mW and can be used when wake-up of less than 600 μs is required. Deep sleep consumes 70 mW and requires 6 ms to wake-up. See the wake-up characteristic in [Figure](#page-15-0) 27. For directions on enabling these modes, see [Table](#page-26-1) 5. The input clock can be in either state when the power-down modes are enabled. The device can enter power-down mode whether using an internal or external reference. However, the wake-up time from light sleep enabled to external reference mode is dependent on the external reference voltage and is not necessarily 0.6 ms, but should be noticeably faster than deep sleep wake-up. No specific power sequences are required.

Layout Information

The evaluation board represents a good model of how to lay out the printed circuit board (PCB) to obtain the maximum performance from the ADS548x. Follow general design rules, such as the use of multilayer boards, a single ground plane for ADC ground connections, and local decoupling ceramic chip capacitors. The analog input traces should be isolated from any external source of interference or noise, including the digital outputs as well as the clock traces. The clock signal traces should also be isolated from other signals, especially in applications such as high IF sampling where low jitter is required. Besides performance-oriented rules, care must be taken when considering the heat dissipation of the device. The thermal heat sink included on the bottom of the package should be soldered to the board as described in the PowerPad Package section. See the ADS548x EVM User Guide on the TI [web](http://www.ti.com) site for the evaluation board schematic.

PowerPAD Package

The PowerPAD package is a thermally-enhanced, standard-size IC package designed to eliminate the use of bulky heat sink and slugs traditionally used in thermal packages. This package can be easily mounted using standard PCB assembly techniques and can be removed and replaced using standard repair procedures.

The PowerPAD package is designed so that the leadframe die pad (or thermal pad) is exposed on the bottom of the IC. This pad design provides an extremely low thermal resistance path between the die and the exterior of the package. The thermal pad on the bottom of the IC can then be soldered directly to the PCB, using the PCB as a heat sink.

Assembly Process

- 1. Prepare the PCB top-side etch pattern including etch for the leads as well as the thermal pad as illustrated in the Mechanical Data section (at the end of this data sheet).
- 2. Place a 6-by-6 array of thermal vias in the thermal pad area. These holes should be 13 mils (0.013 in or 0.3302 mm) in diameter. The small size prevents wicking of the solder through the holes.
- 3. It is recommended to place a small number of 25 mil (0.025 in or 0.635 mm) diameter holes under the package, but outside the thermal pad area, to provide an additional heat path.
- 4. Connect all holes (both those inside and outside the thermal pad area) to an internal copper plane (such as a ground plane).
- 5. Do not use the typical web or spoke via-connection pattern when connecting the thermal vias to the ground plane. The spoke pattern increases the thermal resistance to the ground plane.
- 6. The top-side solder mask should leave exposed the terminals of the package and the thermal pad area.
- 7. Cover the entire bottom side of the PowerPAD vias to prevent solder wicking.
- 8. Apply solder paste to the exposed thermal pad area and all of the package terminals.

For more detailed information regarding the PowerPAD package and its thermal properties, see either the PowerPAD Made Easy application brief [\(SLMA004](http://www.ti.com/lit/SLMA004)) or the PowerPAD Thermally Enhanced Package application report [\(SLMA002](http://www.ti.com/lit/SLMA002)), both available for download at www.ti.com.

The analog input frequency at which the power of the calibrates out the benefit of the board supply fundamental is reduced by 3 dB with respect to the decoupling capacitors.
low-frequency value.

sampling clock and the actual time at which the sampling occurs.

Aperture Uncertainty (Jitter)

The sample-to-sample variation in aperture delay.

The duty cycle of a clock signal is the ratio of the time
the clock signal remains at a logic bigh (clock pulse as the reference, or dBFS (dB to full-scale) when the the clock signal remains at a logic high (clock pulse as the reference, or dBFS (dB to full-scale) when the duration) to the period of the clock signal expressed power of the fundamental is extrapolated to the duration) to the period of the clock signal, expressed converter full-scale range.
as a percentage.

An ideal ADC exhibits code transitions at analog input
 $\begin{array}{c} \text{SINAD} \\ \text{R} \end{array}$ is the some section of all the other spectral components values spaced exactly 1 LSB apart. DNL is the (PS) to the power of all the other spectral components values including noise (P_N) and distortion (P_D) , but excluding deviation of any single step from this ideal value, $\frac{incl}{dc}$ measured in units of LSB.

Common-Mode Rejection Ratio (CMRR)

CMRR measures the ability to reject signals that are presented to both analog inputs simultaneously. The presented to both analog inpute simultaneously. The SINAD is either given in units of dBc (dB to carrier) injected common-mode frequency level is translated information the absolute power of the fundamental is used into dBFS, the spur in the output FFT is measured in as the reference, or dBFS (dB to full-scale) when the dBFS, and the difference is the CMRR in dB.

Effective Number of Bits (ENOB)
ENOB is a measure in units of bits of converter ENOB is ^a measure in units of bits of converter **Temperature Drift** performance as compared to the theoretical limit

Gain error is the deviation of the ADC actual input parameters over the whole temperature range full-scale range function of the whole temperature range function over the range function over the range function over $T_{\text{$ full-scale range from its ideal value, given as a percentage of the ideal input full-scale range. **Total Harmonic Distortion (THD)**

INL is the deviation of the ADC transfer function from. a best-fit line determined by a least-squares curve fit of that transfer function. The INL at each analog input value is the difference between the actual transfer function and this best-fit line, measured in units of THD is typically given in units of dBc (dB to carrier).
LSB.

UITSEL EITOF IS the deviation of output code from the equencies f_1 , f_2) to the power of the worst spectral mid-code when both inputs are tied to component at either frequency $2f_1 - f_2$ or $2f_2 - f_1$).

PSRR is a measure of the ability to reject frequencies

DEFINITION OF SPECIFICATIONS The injected frequency level is translated into dBFS, Analog Bandwidth
The analog input frequency at which the power of the the difference is the PSRR in dB. The measurement
Colibrates out the henefit of the board supply

Signal-to-Noise Ratio (SNR)

Aperture Delay
The delay in time between the rising edge of the input
Aperture of the power of the fundamental (P_S) to the noise floor power (P_N) , excluding the power at dc and in the first five harmonics.

$$
SNR = 10\log_{10} \frac{P_S}{P_N}
$$
 (4)

Clock Pulse Duration/Duty Cycle SNR is either given in units of dBc (dB to carrier)
The duty sycle of a clock signal is the ratio of the time when the absolute power of the fundamental is used

Differential Nonlinearity (DNL)
An ideal ADC exhibits code transitions at analog input
SINAD is the ratio of the power of the fundamental

$$
SINAD = 10\log_{10}\frac{P_S}{P_N + P_D}
$$
 (5)

power of the fundamental is extrapolated to the converter full-scale range.

Temperature drift (with respect to gain error and based on quantization noise:
 $FNOB = (SINAD - 1.76)/6.02$
 F_{MAX} the nominal temperature to the value at T_{MIN} or T_{MAX}.

It is computed as the maximum variation the It is computed as the maximum variation the parameters over the whole temperature range divided

Integral Nonlinearity (INL) THD is the ratio of the power of the fundamental (P_S)
INL is the deviation of the ADC transfer function from to the power of the first five harmonics (P_D) .

$$
\text{THD} = 10\log_{10} \frac{P_S}{P_D} \tag{6}
$$

Two-Tone Intermodulation Distortion (IMD3)
Offset error is the deviation of output code from IMD3 is the ratio of the power of the fundamental (at
mid code when hoth inpute are tied to frequencies f₁, f₂) to the powe mid-code when both inputs are tied to component at either frequency $2f_1 - f_2$ or $2f_2 - f_1$).
Common-mode. IMD3 is given in units of either dBc (dB to carrier) **Power-Supply Rejection Ratio (PSRR)** when the absolute power of the fundamental is used
PSRR is a measure of the ability to reject frequencies as the reference, or dBFS (dB to full-scale) when the power of the fundamental is extrapolated to the present on the power supply. converter full-scale range.

REVISION HISTORY

www.ti.com 7-Oct-2009

PACKAGING INFORMATION

RUMENTS

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details. **TBD:** The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

TEXAS
INSTRUMENTS

PACKAGE MATERIALS INFORMATION

www.ti.com 28-Oct-2009

*All dimensions are nominal

MECHANICAL DATA

NOTES: All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5-1994. А.

- **B.** This drawing is subject to change without notice.
- $C.$ Quad Flatpack, No-leads (QFN) package configuration.
- \bigtriangleup The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.

THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.

Bottom View

NOTE: All linear dimensions are in millimeters

Exposed Thermal Pad Dimensions

RGC (S-PVQFN-N64)

NOTES: A_{-}

- All linear dimensions are in millimeters. B. This drawing is subject to change without notice.
- Publication IPC-7351 is recommended for alternate designs. C.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Application Note, Quad Flat-Pack Packages, Texas Instruments Literature No. SLUA271, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com>.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC 7525 for stencil design considerations.
- F. Customers should contact their board fabrication site for recommended solder mask tolerances and via tenting recommendations for vias placed in thermal pad.

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